ELEN E4810: Digital Signal Processing Topic 9: Filter Design: FIR

- 1. Windowed Impulse Response
- 2. Window Shapes
- 3. Design by Iterative Optimization



1. FIR Filter Design

FIR filters

- no poles (just zeros)
- no precedent in analog filter design
- Approaches
 - windowing ideal impulse response
 - iterative (computer-aided) design



Least Integral-Squared Error • Given desired FR $H_d(e^{j\omega})$, what is the best finite $h_t[n]$ to approximate it? best in what sense?

Can try to minimize Integral Squared Error (ISE) of frequency responses:

$$\phi = \frac{1}{2\pi} \int_{-\pi}^{\pi} \left| H_d(e^{j\omega}) - H_t(e^{j\omega}) \right|^2 d\omega$$

 $= \text{DTFT}\{h_t[n]\}$

Least Integral-Squared Error

- Ideal IR is h_d[n] = IDTFT{H_d(e^{jω})}, (usually infinite-extent)
- By Parseval, ISE $\phi = \sum_{n=-\infty} |h_d[n] h_t[n]|^2$
- But: $h_t[n]$ only exists for n = -M..M,

 $\Rightarrow \phi = \sum_{n=-M}^{M} |h_d[n] - h_t[n]|^2 + \sum_{n<-M, n>M} |h_d[n]|^2$ minimized by making $h_t[n] = h_d[n], -M \le n \le M$ not altered by $h_t[n]$

Least Integral-Squared Error

Thus, minimum mean-squared error approximation in 2M+1 point FIR is truncated IDTFT:

$$h_t[n] = \begin{cases} \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) e^{j\omega n} d\omega & -M \le n \le M \\ 0 & \text{otherwise} \end{cases}$$

■ Make causal by delaying by *M* points → $h'_t[n] = 0$ for n < 0









Gibbs Phenomenon

Truncated ideal filters have Gibbs' Ears:

Increasing filter length → narrower ears (reduces ISE) <u>but</u> height the same

→ **not** optimal by minimax criterion



Where Gibbs comes from
• Truncation of
$$h_d[n]$$
 to $2M+1$ points is
multiplication by a rectangular window:
 $h_t[n] = h_d[n] \cdot w_R[n]$
 $w_R[n] = \begin{cases} 1 & -M \le n \le M \\ 0 & \text{otherwise} \end{cases}$

Multiplication in time domain is convolution in frequency domain:

$$g[n] \cdot h[n] \leftrightarrow \frac{1}{2\pi} \int_{-\pi}^{\pi} G(e^{j\theta}) H(e^{j(\omega-\theta)}) d\theta$$



Where Gibbs comes from

Thus, FR of truncated response is convolution of ideal FR and FR of rectangular window (pd.sinc):



Where Gibbs comes from

Rectangular window:

$$w_R[n] = \begin{cases} 1 & -M \le n \le M \\ 0 & \text{otherwise} \end{cases} \implies \begin{aligned} W_R(e^{j\omega}) &= \sum_{n=-M}^M e^{-j\omega n} \\ &= \frac{\sin(2M+1)\frac{\omega}{2}}{\sin\frac{\omega}{2}} \end{aligned}$$

Mainlobe width
 (∝ 1/L) determines
 transition band
 Sidelobe height
 determines ripples
 ≈ invariant



with length

2. Window Shapes for Filters

- Windowing (infinite) ideal response → FIR filter: $h_t[n] = h_d[n] \cdot w[n]$
- Rectangular window has best ISE error
- Other "tapered windows" vary in:
 - mainlobe \rightarrow transition band width
 - sidelobes \rightarrow size of ripples near transition
- Variety of 'classic' windows...



Window Shapes for FIR Filters





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Window Shapes for FIR FiltersComparison on dB scale:



Dan Ellis

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²⁰¹³⁻¹¹⁻²⁰

Adjustable Windows

- So far, discrete main-sidelobe tradeoffs..
- Kaiser window = parametric, continuous tradeoff: modified zero-order $w[n] = \frac{I_0(\beta \sqrt{1 - (\frac{n}{M})^2})}{V[n]} -M \le n \le M$ Bessel function
 - \blacksquare Empirically, for min. SB atten. of α dB:

$$\beta = \begin{cases} 0.11(\alpha - 8.7) & \alpha > 50 \\ 0.58(\alpha - 21)^{0.4} + 0.08(\alpha - 21) & 21 \le \alpha \le 50 \\ 0 & \alpha < 21 \end{cases} \xrightarrow{\text{order}} N = \frac{\alpha - 8}{2.3\Delta\omega} \\ \text{transition} \\ \frac{\text{width}}{\alpha} \end{cases}$$

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Windowed Filter Example

- Design a 25 point FIR low-pass filter with a cutoff of 600 Hz (SR = 8 kHz)
- No specific transition/ripple req's
 → compromise: use Hamming window
- Convert the frequency to radians/ sample: $\omega_c = \frac{600}{8000} \times 2\pi = 0.15\pi$

600 cyc/sec / 8000 samp/sec x 2π rad/cyc = 0.15π rad/samp



Windowed Filter Example

- 1. Get ideal filter impulse response: $\omega_c = 0.15\pi \implies h_d[n] = \frac{\sin 0.15 \pi n}{\pi n}$
- 2. Get window: Hamming (a) $N = 25 \rightarrow M = 12$ (N = 2M+1) $\Rightarrow w[n] = 0.54 + 0.46 \cos\left(2\pi \frac{n}{25}\right) \quad -12 \le n \le 12$ 3. Apply window: 0.15 h[n] 0.05 $h[n] = h_d[n] \cdot w[n]$ 0 -20 -10 0 10 n $= \frac{\sin 0.15 \,\pi n}{\pi n} \left(0.54 + 0.46 \cos \frac{2 \,\pi n}{25} \right)$ $-12 \le n \le 12$

Freq. Resp. (FR) Arithmetic

• Ideal LPF has pure-real FR i.e. $\theta(\omega) = 0, H(e^{j\omega}) = |H(e^{j\omega})|$



3. Iterative FIR Filter Design

Can derive filter coefficients by iterative optimization:



Gradient descent / nonlinear optimiz'n



Error Criteria

$$\varepsilon = \int_{\omega \in R} |W(\omega) \cdot [D(e^{j\omega}) - H(e^{j\omega})]|^{p} d\omega$$
error
measurement
region
weighting response

$$\varepsilon \to minimax$$

$$\psi(\omega)$$

$$\psi(\omega)$$

$$W(\omega)$$

$$\psi(\omega)$$

$$\psi(\omega)$$

$$\psi(\omega)$$

$$W(\omega)$$

$$\psi(\omega)$$

Minimax FIR Filters

- Iterative design of FIR filters with:
 - equiripple (minimax criterion)
 - Iinear-phase

→ symmetric IR h[n] = (-)h[-n]

• Recall: Symmetric FIR filters have FR $H(e^{j\omega}) = e^{-j\omega M} \tilde{H}(\omega)$ with pure-real \tilde{H} $\tilde{H}(\omega) = \sum_{k=0}^{M} a[k] \cos(k\omega) \quad \begin{array}{l} a[0] = h[M] \\ a[k] = 2h[M - k] \end{array}$

i.e. combo of cosines of multiples of ω

order 2M)

n

Minimax FIR Filters $\tilde{H}(\omega) = \sum_{k=0}^{M} a[k] \cos(k\omega)$

Now, cos(kω) can be expressed as a polynomial in cos(ω)^k and lower powers

• e.g. $\cos(2\omega) = 2(\cos\omega)^2 - 1$

Thus, we can find α s such that $\tilde{H}(\omega) = \sum_{k=0}^{M} a[k] cos(k\omega) = \sum_{k=0}^{M} \alpha[k] (cos\omega)^{k}$ K = 0 $M^{th} order$ K = 0 $M^{th} order$ K = 0 $M^{th} order$ K = 0

• $\alpha[k]$ s easily lead to a[k]s





Alternation Theorem

- $\tilde{H}(\omega)$ is the unique, best, weightedminimax order 2*M* approx. to $D(e^{j\omega})$
- $\Leftrightarrow \quad \text{For "extremal" freqs} \\ \omega_0 < \omega_1 < \ldots < \omega_M < \omega_{M+1} \text{ over } \omega \text{ subset } R$
 - Error magnitude is equal at each extrema: $|\varepsilon(\omega_i)| = \varepsilon \quad \forall i$

Peak error alternates in sign: $\varepsilon(\omega_i) = -\varepsilon(\omega_{i+1})$

• $\tilde{H}(\omega)$ has at least *M*+2 "extremal" freqs

Alternation Theorem

Hence, for a frequency response:



- If ε(ω) reaches a peak
 error magnitude ε at
 some set of extremal
 frequences ω_i
- And the sign of the peak error alternates
- And we have at least M+2 of them
- Then optimal minimax



Alternation Theorem

- By Alternation Theorem, M+2 extrema of alternating signs
 ⇒ optimal minimax filter
- **<u>But</u>** $\tilde{H}(\omega)$ has at most *M*-1 extrema \Rightarrow need at least 3 more from band edges
- 2 bands give 4 band edges ⇒ can afford to "miss" only one
- Alternation rules out transition band edges, thus have 1 or 2 outer edges



Alternation Theorem • For M = 5 (10th order):

- 8 extrema (M+3,
 4 band edges)
 - great!
- 7 extrema (*M*+2,
 3 band edges)
 - OK!
- 6 extrema (*M*+1, only 2 transition band edges)
 → NOT OPTIMAL



Parks-McClellan Algorithm

To recap:

- FIR CAD constraints $D(e^{j\omega}), W(\omega) \rightarrow \varepsilon(\omega)$
- Zero-phase FIR $\tilde{H}(\omega) = \sum_k \alpha_k \cos^k \omega \rightarrow M-1 \min/\max$
- Alternation theorem **optimal** → $\ge M+2$ pk errs, alter'ng sign
- Hence, can spot 'best' filter when we see it but how to find it?



Parks-McClellan Algorithm

- Alternation $\rightarrow [\widetilde{H}(\omega) \widetilde{D}(\omega)]/W(\omega)$ must = ± ε at *M*+2 (unknown) frequencies { ω_i }...
- Iteratively update h[n] with Remez exchange algorithm:
 - estimate/guess M+2 extremals { ω_i }
 - solve for $\alpha[n], \varepsilon (\rightarrow h[n])$
 - find actual min/max in $\varepsilon(\omega) \rightarrow \text{new} \{\omega_i\}$
 - repeat until $|\varepsilon(\omega_i)|$ is constant
- Converges rapidly!







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Dan Ellis

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